

UNITED STATES PATENT APPLICATION

**WAFER LEVEL BURN-IN AND ELECTRICAL
TEST SYSTEM AND METHOD**

Inventor(s): Donald Paul Richmond II, Citizen of United States, Residing in
Palo Alto, California
John Dinh Hoang, Citizen of United States, Residing in San Jose,
California
Jerzy Lobacz, Citizen of United States, Residing in San Mateo,
California

Assignee: Aehr Test Systems
400 Kato Terrace
Fremont, CA 94539



Wilson Sonsini Goodrich & Rosati
650 Page Mill Road
Palo Alto, CA 94304
(650) 493-9300
(650) 493-6811

WAFER LEVEL BURN-IN AND ELECTRICAL TEST SYSTEM AND METHOD

5

ORIGIN OF THE INVENTION

This invention was supported in part by grants from DARPA. The U.S. Government may have rights in this invention.

10 **BACKGROUND OF THE INVENTION**1. Field of the Invention:

The present invention relates generally to a system and method for evaluation of integrated circuits and other semiconductor devices. More particularly, it relates a system
15 incorporating hardware and suitable interconnections which allow efficient burn-in testing of a multiplicity of semiconductor devices while still incorporated in a semiconductor wafer. This invention is related to the inventions in commonly owned U.S. Patent 5,429,510, issued to Barraclough et al. on July 5, 1995, entitled "High-Density Interconnect Technique," and commonly owned U.S. Patent 5,682,472, issued to Brehm et al. on October 28, 1997 and
20 entitled "Method and System for Testing Memory Programming Devices," the disclosures of which are hereby incorporated by reference herein. This invention is further related to the invention in a concurrently filed, copending, commonly owned application filed in the names of Frank O. Uher, Mark C. Carbone, John W. Andberg and Donald P. Richmond II, entitled "Wafer Level Burn-In and Test Cartridge" (Attorney Docket No. AEHR-006/00US), the
25 disclosure of which is also incorporated by reference herein.

2. Description of the Prior Art:

When fabrication of integrated circuits and other semiconductor devices has been completed, the semiconductor devices are subjected to burn-in and electrical tests in order to identify and eliminate defective semiconductor devices before shipment to a customer. The
30 term "burn-in" relates to operation of an integrated circuit at a predetermined temperature or temperature profile, typically an elevated temperature in an oven, a reduced temperature in an environmentally controlled enclosure, or a combination of an elevated temperature followed by a reduced temperature. Certain operating electrical bias levels and/or signals are supplied to the semiconductor devices while they are at the elevated temperature. The use of the
35 elevated temperature or the combination of an elevated temperature followed by a reduced

temperature accelerates stress to which the devices are subjected during burn-in, so that marginal devices that would otherwise fail shortly after being placed in service fail during burn-in and are eliminated before shipping. In electrical test, a more complete set of operating electrical bias levels and signals are supplied to the device to provide a thorough evaluation of its functions.

As is apparent from the Brehm et al. patent, there are a variety of burn in and electrical test systems known in the art for burn-in and electrical test of integrated circuits and other semiconductor devices. To date, most of the prior art systems carry out the burn-in and electrical test after the integrated circuits have been separated into individual chips or die from a wafer in which they have been manufactured.

More recently, interest has developed in wafer-level burn-in systems, some of which systems also include electrical test capability. In these systems, the integrated circuits undergo burn-in and may undergo electrical test prior to separation into individual integrated circuit chips.

Wafer-level burn-in systems have attracted interest because they allow defective integrated circuits to be identified by the burn-in process before additional expense is incurred in their handling and packaging. Similarly, it is desirable to carry out electrical test of the integrated circuits while they are still in wafer form. Electrical test involves applying a suite of electrical signal inputs to each integrated circuit to make sure that it performs properly for its intended use.

While the ability to carry out both burn-in and electrical test in a single wafer-level system is a highly desired result, there are significant interconnection, signal supply and power supply problems to be overcome before such a system can be implemented in practice. In a preferred implementation, the present invention is directed to solving those problems. In its broadest form, aspects of the present invention may, however, be employed in a system that carries out wafer-level burn-in or wafer-level electrical test alone.

SUMMARY OF THE INVENTION

In accordance with one aspect of the invention, a burn-in test system includes a device under test zone configured to receive a plurality of cartridges each containing a semiconductor wafer including a plurality of integrated circuits. Each of the plurality of cartridges includes a rigid probe signal printed circuit board and a probe power printed circuit board substantially parallel to and closely spaced from the rigid probe printed circuit board. Test electronics are positioned adjacent to the device under test zone. Power electronics are

positioned adjacent to said device under test zone. A first interconnection system connects the test electronics to the rigid probe signal printed circuit board. A second interconnection system connects the power electronics to the probe power printed circuit board. The first and second interconnection systems are arranged in a stacked relationship. The probe power printed circuit board has at least a bendable section permitting a portion of the probe power printed circuit board to be spaced a greater distance away from the rigid probe signal printed circuit board proximate to the second interconnection system.

In accordance with a second aspect of the invention, a test system includes a device under test zone configured to receive a plurality of cartridges each containing a semiconductor wafer including a plurality of integrated circuits. Each of the plurality of cartridges includes a rigid probe signal printed circuit board and a probe power printed circuit board substantially parallel to and closely spaced from the rigid probe printed circuit board. Test electronics are positioned adjacent to said device under test zone. Power electronics are positioned adjacent to the device under test zone. A first interconnection system connects the test electronics to the rigid probe signal printed circuit board. A second interconnection system connects the power electronics to the probe power printed circuit board. The first and second interconnection systems are arranged in a stacked relationship. The probe power printed circuit board has at least a bendable section permitting a portion of the probe power printed circuit board to be spaced a greater distance away from the rigid probe signal printed circuit board proximate to the second interconnection system.

In a third aspect of the invention, a burn-in system has a temperature controlled zone configured to receive a plurality of cartridges each containing a semiconductor wafer including a plurality of integrated circuits. Test electronics are positioned in a cool zone. Power electronics are positioned in the cool zone. A transition zone separates the temperature controlled zone and the cool zone.

In a fourth aspect of the invention, a test system includes a device under test zone configured to receive a plurality of cartridges each containing a semiconductor wafer including a plurality of integrated circuits. Test electronics on a first circuit board are positioned adjacent to the device under test zone. Power electronics on a second circuit board are positioned adjacent to said device under test zone. Each of the plurality of cartridges are connected to the test electronics by a first connection between one of the plurality of cartridges and the first circuit board and to the power electronics by a second connection between the one of said plurality of cartridges and the second circuit board separate from the first connection.

In a fifth aspect of the invention, a test system includes a first plurality of test channels each adapted to receive a second plurality of integrated circuits under test. A second plurality of power modules are each connected to one of the integrated circuits under test in each test channel. A controller is connected and configured for successive selection of one of the first plurality of test channels.

In a sixth aspect of the invention, a method for burn-in testing integrated circuits in wafer form includes providing a temperature controlled zone configured to receive a plurality of cartridges each containing a semiconductor wafer including a plurality of integrated circuits. The integrated circuits are tested with test electronics positioned in a cool zone. Power is provided to the integrated circuits with power electronics positioned in the cool zone. The test and power electronics are separated from the temperature controlled zone with a transition zone between the temperature controlled zone and the cool zone.

In a seventh aspect of the invention, a method for testing integrated circuits in wafer form includes connecting a first plurality of integrated circuits in a second plurality of test channels. A first plurality of power modules is connected to one of the integrated circuits under test in each test channel. One of the second plurality of test channels is selectively selected. The first plurality of the integrated circuits in the selected test channel is tested. The selective selection and testing steps are repeated until all of the integrated circuits have been tested.

In reviewing the following more detailed description and drawings of the present invention, the advantages and features of the invention should be more readily apparent to those skilled in the art.

BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 is a block diagram and schematic representation of an embodiment of a burn-in and electrical test system in accordance with the invention.

Figure 2 is a block diagram and schematic representation of part of the system shown in Figure 1.

Figure 3 is another more detailed block diagram and schematic representation of the part of the system shown in Figure 2.

Figure 4 is a partially exploded block diagram of the part of the system shown in Figure 3.

Figure 4A is a cross section view of an interconnection system used in the part of the system portion shown in Figure 2.

Figure 5 is a block diagram of another part of the system shown in Figures 1-4.

Figures 6 and 7 are circuit diagrams of a portion of the system part of Figure 5.

Figures 8 and 9 are pinout connection diagrams of integrated circuits under burn-in and test using the invention.

5 Figures 10 and 11 are somewhat schematic representations of interconnections used in the system portion shown in Figures 2-4.

Figure 12 is a cross section view of a portion of the interconnections shown in Figure 10.

Figure 13 is a plan view of a portion of the interconnections shown in Figure 10.

10 Figure 14 is a cross section view of a portion of the interconnections shown in Figure 11.

Figure 15 is a cross section view of one of the interconnections in the system portion shown in Figures 2-4.

15 Figures 16A, 16B and 16C are perspective, top and side views of a part of the interconnection shown in Figure 15.

DETAILED DESCRIPTION OF THE INVENTION

Turning now to Figure 1, there is shown a burn-in and electrical test system 20 in accordance with the invention. As shown, a local controller 21 is connected to a plurality of electrical test zones #1 through #n via an internal Ethernet network 101. Electrical test zone #1 shows the details of each electrical test zone. Each of the electrical test zones has a single test pattern generator 103 connected by a parallel bus 105 to a plurality of test slots 107 comprising a test slot interface 119. Each test slot 107 comprises optional fault analysis 109, a driver comparator board 111 and a wafer/die power system 113. Two separate connections for each wafer test cartridge 26 for test electronics and for power distribution are represented at 115 and 117. The optional fault analysis 109 and driver comparator board 111 comprise the test electronics and are connected to the wafer test cartridge 26 by connection 115. The wafer/die power system 113 is connected to the wafer test cartridge 26 by connection 117.

Figure 2 shows a portion of the system 20 of Figure 1. A plurality of wafer cartridges 26 are connected to test electronics 28 and power electronics 30. The test electronics 28 comprises a single pattern generator printed circuit board (PCB) 29 and separate signal driver and fault analysis PCBs 33 for each wafer cartridge 26. Each of the wafer cartridges 26 contains a semiconductor wafer incorporating a plurality of integrated circuits. All of the signal driver and fault analysis PCBs 33 are connected to the pattern generator PCB by parallel bus 105. Further details of the cartridges 26 are contained in a concurrently filed, co-

owned pending application entitled "Wafer Level Burn-In and Test Cartridge and Alignment Method," filed in the names of Frank O. Uher, Mark C. Carbone, John W. Andberg and Donald P. Richmond II (Attorney Docket No. AEHR-006/00US), the disclosure of which is hereby incorporated by reference herein. Some aspects of the cartridge 26 will be described below as necessary for a more complete understanding of the present invention.

Figures 3 and 4 show further details of the wafer cartridge 26, test electronics 28 and power electronics 30 and how they are interconnected. As shown in Figure 3, the test electronics 28 consists of a pattern generator PCB 29 and a signal driver and fault analysis PCB 33 connected together by the parallel bus 105. The fault analysis PCB 33 is connected to a rigid signal probe PCB 104 in cartridge 26 through a driver extender PCB 102 to provide a straight through signal path. The probe PCB 104 is rigid in order to allow close control of impedance between each signal line and a backplane, to be discussed more fully below in connection with Figures 10, 12 and 13, thus providing impedance controlled interconnections between a semiconductor wafer under test and the test electronics 28.

The portion of the system 20 shown in Figures 3 and 4 is divided into a temperature controlled zone 22, a cool or ambient temperature zone 24 and a transition zone 25. The temperature controlled zone is either heated to an elevated temperature, such as 150°C, or chilled, such as to a temperature of 0°C. during the burn-in or test operation. The wafer cartridge 26 extends from the temperature controlled zone 22 into the transition zone 25. A thermal dam 156 is positioned around the wafer cartridge 26 at the interface between the temperature controlled zone and the transition zone to minimize heat transfer between the zones around the cartridge 26. The transition zone 25 is provided in order to prevent heat or cold leakage from the controlled temperature zone into the signal driver and fault analysis PCB 33. Such heat or cold leakage would change the temperature of the PCB 33 over time, thus causing a performance change, resulting in a variation of test conditions over time. Additionally, cold leakage into the PCB 33 would result in condensation or thermal damage to the PCB 33.

The driver extender PCB 102 serves to space the signal driver and fault analysis PCB 33 from the temperature controlled zone 22 and the transition zone 25 for further heat and cold isolation. Additionally, the driver extender PCB 102 permits impedance matching of the signal probe PCB and the signal driver and fault analysis PCB 33. In practice, the signal probe PCB 104 has an impedance of about 50 ohm, and the signal driver and fault analysis PCB 33 has an impedance of about 28 ohm. The driver extender PCB has a varying impedance along its length, from about 28 ohm on the signal driver and fault analysis PCB 33

end to about 50 ohm on the signal probe PCB 104 end. This impedance matching permits higher quality signals to be transmitted between the signal driver and fault analysis PCB 33 and the signal probe PCB 104.

The power distribution system 30 is connected to a probe power PCB 106 in the cartridge 26. The probe PCB 106 has a flexible portion 107 order to allow it to be positioned closely adjacent to and parallel with the rigid probe PCB 104 along most of its extent in the cartridge 26, yet extend a substantial distance away from the probe PCB 106 at its interconnection with the power distribution system 30.

The cartridge 26 is connected to the test electronics 28 and the power distribution system 30 through a mini-backplane PCB 108. High pin density connectors 109 are used to connect the cartridge 26 to the driver extender PCB 102 and to the power distribution system 30. The connectors 109 include a total of 4200 pin connections, compared with a total of 680 pin connections in the system described in the above-referenced Brehm et al. patent. The connectors have insulated pins and the signal pins are set in an electromagnetic interference (EMI) shield housing. Suitable high pin density connectors 109 of this type are commercially available from AMP Incorporated, Harrisburg, Pennsylvania and will not be further described herein.

The power distribution system 30 includes a die power main PCB 110 and a set of 32-channel die power dual-in-line modules (DIMs) mounted on the die power main PCB 110. In the test electronics 28, the driver extender board 102 is connected to a main signal driver PCB 33 by an interconnection system 31. A set of signal driver DIMs and a fault analysis PCB 114 are mounted on the main signal driver PCB 33.

Figure 4A shows details of the interconnection 31. This interconnection system is the subject of the above-referenced Barraclough et al. patent.

The system 31 employs contact fingers 32 on both surfaces 34 and 36 of PCB 102 and PCB 33. Each of the PCBs 102 and 33 has a card-edge connector 44 and 46. The contact fingers 32 and the card-edge connectors 44 and 46 of each PCB mate inversely with each other on adjacent PCBs, i.e., the card-edge connector 44 of the PCB 102 mates with contact fingers 32 of the PCB 33, and the card-edge connector 46 of the PCB 33 mates with the contact fingers of the PCB 102. The PCB 102 has two sets 70 and 72 of interconnections connected to metal contacts 74 of the card-edge connector 44 and two sets of 76 and 78 of interconnections connected to contact fingers 32 of the PCB 33. Similarly, PCB 33 has two sets 80 and 82 of interconnections connected to contact fingers 32 of the PCB 33 and two sets 84 and 86 of interconnections connected to metal contacts 88 of the card-edge connector 46.

With this interconnection system 31 there is twice the density of interconnects per inch using the same card-edge connector compared with a typical prior art interconnection system. for example. 40 interconnects per inch of card edge between two PCBs, compared with 20 interconnects per inch in the prior art example.

Besides doubling the number of interconnects, the interconnection system 31 is self-aligning. The card-edge connectors 44 and 46 are each set back from the contact fingers of their respective PCBs 38 and 40. Using PCBs 38 and 40 of the same thickness and using connectors 44 and 46 with identical geometry that are mounted directly on the PCBs for both PCBs that are connected together, all dimensional relationships are maintained when the assembly is inverted for the second connection. Connector support bars 90 are provided, fixedly attached (such as bolted) on each PCB 38 and 40 behind the connectors 44 and 46 to provide sufficient structural rigidity and support for plugging and unplugging the connectors 44 and 46.

Figure 5 shows the parallel test processing capability and segmented power distribution of the system 20. Each power module 280 is connected to 32 devices under test 200 comprising 32 channels. While carrying out the testing, only one of the 32 channels is made active at a time using the chip select lines 282. This means that only one device under test 200 is powered by each power module 280 at a time, thus resulting in far less need for capacitance per power module 280. In practice, power is supplied to all of the devices 200 under test in their inactive state, but only one device per power module is powered to its active state at a time. The active state uses power at a much higher level and makes much more electrical noise on the power lines. The capacitance in each power module is provided to satisfy current demand when cycling from low to high power demand at high frequencies. There are a total of 32 power modules, but only 8 are shown in Figure 10. This segmented mode of power distribution is far more manageable than attempting to power all of the devices under test at once.

Figure 6 shows a circuit schematic of the power module 280. The power module 280 has a microcontrol element 252 connected at 254 to control turning on and turning off an MOS FET power switch 256. The microcontrol element 252 can be implemented as an microcontroller, a field programmable gate array (FPGA) or a Cypress programmable logic device (CPLD). A Vdd input 253 is connected to input 255 of the power switch 256. Output 258 of the power switch 256 is connected to the device under test (DUT) 200. The microcontrol element 252 is also connected to an analog to digital (A/D) converter 260 by an A/D bus 262, to a channel multiplexer 264 by a multiplexed bus 266 and to a voltage –

current measurement multiplexer 268 by the multiplexed bus 266. Input 270 of the A/D converter 260 is connected to the voltage – current measurement multiplexer 268. Outputs 272 of the channel multiplexer 264 are connected through an instrumentation amplifier 274 to the voltage – current multiplexer 268. One of the outputs 272 on the DUT 200 side of R connects directly to the voltage – current multiplexer 268. The microcontrol element 252 is connected by a microprocessor bus 276 to a microprocessor on the signal driver PCB 33. (see also Figures 2-4). That microprocessor is an intermediate level of control between the microcontrol element 252 and another microprocessor in the local controller 21 (Figure 1). An asynchronous clock input 255 is connected to the microcontrol element 252.

In operation, the microcontrol element 252 controls the supply of power to the devices 200 under test by sequencing the channel multiplexer 264 through channels 1-32 (see also Figure 5). When each DUT 200 is powered, the microcontrol element controls the voltage – current multiplexer 268 to cycle between voltage and current measurements. The voltage and current inputs from the DUT 200 are supplied through the channel multiplexer to the voltage – current multiplexer 268. The A/D converter 260 converts to digital, and the microcontrol element 252 receives, the voltage and current measurements and compares those measurements against the programmed high and low limits in order to detect an under or over voltage or under or over current condition. When any is detected, the power switch 256 is turned off before damage to a probe contacting the DUT 200 can take place. The significance of local control by the microcontrol element 252 is its speed of operation. The two measurements to detect voltage and current take place within the time of about 3 milliseconds it takes power switch 256 to switch from an off to an on state. This speed of operation protects the wafer DUT 200 and the wafer probe either when failure of the DUT 200 takes place while it is under test or when the device first turns on.

Figure 7 shows another embodiment of a power module 280 in the form of a power regulator control and voltage/current readback circuit 210. A V_{dd} reference input 212 is supplied through resistor network 214 to power control transistor T1 and adjust input 216 of an adjustable regulator integrated circuit 218. A raw power input 219 is also connected to the integrated circuit 218. Output 220 of the integrated circuit 218 is connected to the device under test 200. An output 236 of the microcontrol element 252 is connected through resistor network 238 to the base of power control transistor T1. In operation, the adjustable regulator 218 attempts to adjust the raw power input at 219 to be equal to the reference at 216. When the power control transistor T1 is turned on by the microcontrol element 252, transistor T1 pulls down the adjust input 216 to the adjustable regulator integrated circuit 218, shutting it

off. The circuit 210 allows custom regulation of the test voltage to each DUT 200, thus improving the accuracy of the test voltage to each device. Other than as shown and described, the construction and operation of the Figure 7 circuit is the same as that of the Figure 6 circuit.

Figures 8 and 9 respectively show an example of signal and power connections to a Rambus dynamic random access memory (RDRAM) integrated circuit 200 and a general example of a memory integrated circuit 200 on a semiconductor wafer. As shown, connections 202 include a capacitance of 0.1 to 5 μ farad for each connection. Connections 204 and two of the interconnections 202 include a resistance of 200 to 800 ohm for each connection. Connections 206 include a resistance of 20 to 80 ohm. The resistances R and R1 are provided for isolation to allow tolerating failure of any one integrated circuit 200 under test of a semiconductor wafer. The difference between R and R1 is because the integrated circuits 200 under test have a low ability to drive capacitance and the resistance R1 therefore needs to be lower to give an appropriate RC constant. In the interconnections of the cartridge 26 and the various PCBs, the connections to the integrated circuit 200 are bussed together as indicated.

Further details of the wafer cartridge 26 are shown in Figures 10-14. A probe 150 is centrally disposed on the probe PCB 104. The probe 150 has a plurality of tiles 152 that contain a multiplicity of contacts (not shown) for contacting each of the integrated circuits in a semiconductor wafer. The probe 150 is mounted on a contactor 151. When the wafer cartridge is loaded into the burn-in and electrical test system (see Figures 2-4), the portions 154 of the interconnections 109 (see also Figures 3 and 4) that is attached to the cartridge 26 attach to the rest of interconnections 109 on the mini-backplane PCB 108. The signal connections in the portion 154 comprise insulated pins that are set in an electromagnetic interference (EMI) shield housing. Flexible interconnections 158 electrically connect the contactor 151 to the signal probe PCB 104 and the power probe PCB 106. Since the contactor 151, the probe signal PCB 104 and the probe power PCB 106 are rigid and are made of different materials, the flexible interconnections 158 allow for differential expansion of the probe 150, probe signal PCB 104 and probe power PCB 106 when they are heated during burn-in.

Figures 12 and 13 show details of the signal probe PCB. Signal lines 300 are disposed on one side of a 1X thickness dielectric core 302, with a power or ground plane 304 on the other side of the dielectric core 302. The signal lines 300 are spaced from 3X to 6X

horizontal distance apart from one another. In the layers, the signal lines are spaced a vertical distance of 3X to 6X from an adjacent power or ground plane 304 associated with another set of signal lines 300 by dielectric and glue layer 306. Adjacent power or ground planes 304 are spaced a multiple of X distance vertically from each other by dielectric and glue layer 308.

5 Adjacent signal lines 300 associated with different power or ground planes 304 are spaced apart a distance of 6X vertically from one another by dielectric and glue layer 310. These spacing relationships minimize cross talk between adjacent conductors, and in the case of the thin separation between signal lines 300 and their associated power or ground planes 304, the dielectric core 302 is thin in order to improve AC performance.

10 Details of the power probe PCB 106 are shown in Figure 14. The power probe PCB 106 is rigid, except for the bendable section 107 that allows the power probe PCB 106 to be spaced away from the probe signal PCB 104 near the connections 109 (see also Figure 3). The power probe PCB 106 has a coverlay 320 on its top and bottom. Moving inward from the top and bottom, conductors 322 and 324 are respectively adjacent to the coverlays 320.

15 The conductors 322 and 324 are separated from conductors 326 and 328 by glue layers 330 and 332. Conductors 326 and 328 are separated from conductors 334 and 336 by dielectric layers 338 and 340. Conductors 334 and 336 are separated from conductors 342 and 344 by glue layers 346 and 348, except in the bendable section 107, where the conductors 334 and 336 are separated from conductors 342 and 344 by voids 350 and 352. The voids 350 and

20 352 permit the bendable section 107 to flex. The conductors 342 and 344 are separated from each other by dielectric layer 354.

Figures 15-16C show a copper ground lug 400 used for a ground connection to the PCBs 104 and 106, which are connected together by a high density board to board connector 402. Alternate pins 404 of the connector 402 are for signals and power. The presence of the

25 ground lug 400 connected to traces on each board provides a good ground for both boards 104 and 106, so that every third pin of the board to board connector does not need to be used for ground, as in the prior art. The high density board to board connector 402 is implemented with a quad row staggered SMT socket assembly obtainable from Samtec USA, New Albany, Indiana, under the designation SMT Socket Assembly. A similar SMT terminal assembly is

30 also used to connect flexible leads 158 (Figure 10) to the PCB 104. The ground lug has surface mount leads 406 and through hole post leads 408. The through hole post leads 408 serve to hold the two boards in registry with one another and allow screw 410 to be tightened without shearing the surface mount leads 406 from the boards 104 and 106. The ground lug 400 is also matched in height to the height of the board to board connector 402. The ground

lug therefore optimizes the use of the high density connector 402 and gives a good mechanical restraining device matched in height to the mating connector set.

It should be apparent to those skilled in the art that various changes in form and details of the invention as shown and described may be made. It is intended that such
5 changes be included within the spirit and scope of the claims appended hereto.